



Pre normative research  
on the indoor use of fuel cells and hydrogen systems

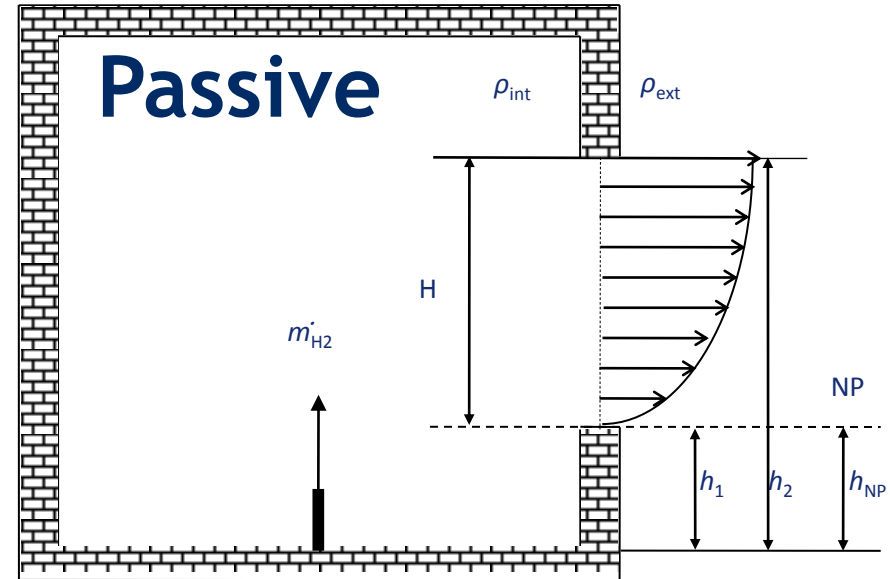
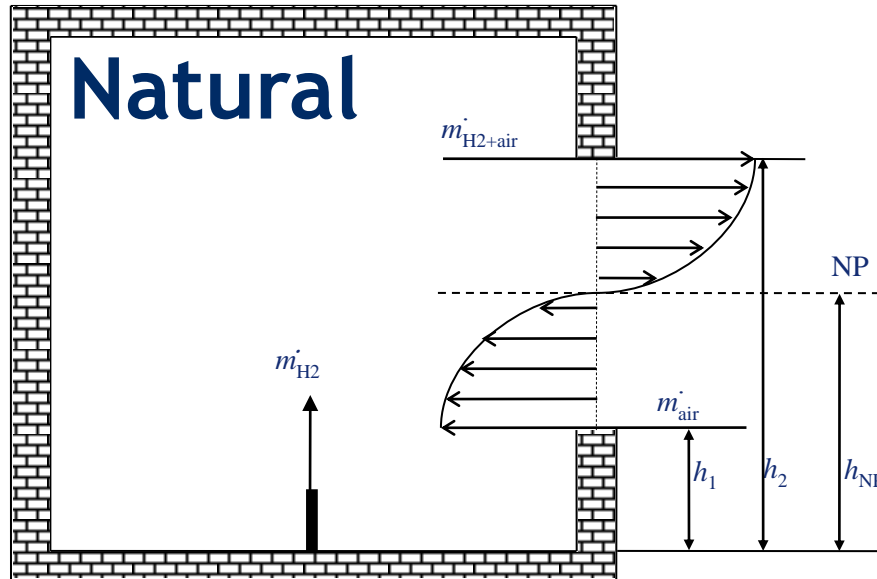
# Passive and forced ventilation systems with one vent

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# General strategies

- Vertically stretched vents (Height > Width) are more efficient than horizontally stretched of the same area
- Ventilation system with two vents at the different heights is more effective than a system with one vent of the same area. The larger difference in vent heights is, the more efficient is ventilation system
- Vents on the vertical walls are more efficient than vents in (horizontal) roof
- Multiple vents located at all sides of enclosure at different heights improve ventilation for all wind directions
- Obstruction (grills, rain covers), and horizontal ducts reduce vent efficiency



- **Natural ventilation** equations for air ventilation in buildings are derived in the assumption of equality of flow in and out (neutral plane is at half vent height).
- **Passive ventilation:** neutral plane for lighter than air gases can be anywhere below half of a vent height.

# Natural versus passive 1/2

Natural ventilation:

$$X = \left[ \frac{Q_0}{C_D A (g' H)^{1/2}} \right]^{2/3}$$

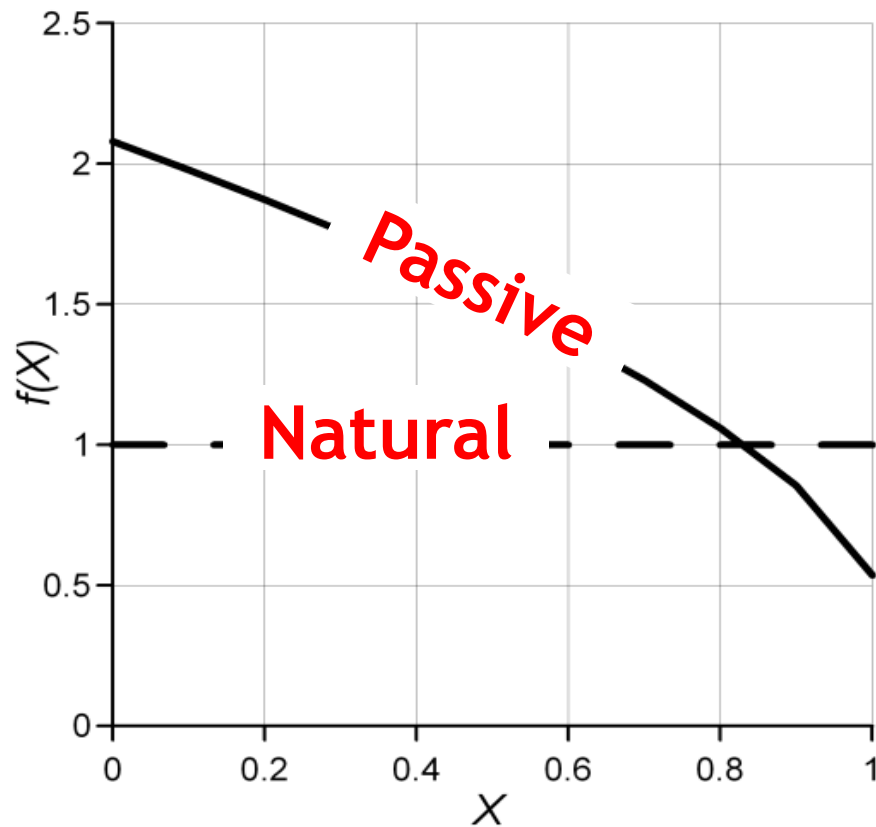
Passive ventilation:

$$X = f(X) \cdot \left[ \frac{Q_0}{C_D A (g' H)^{1/2}} \right]^{2/3}$$

Difference:  $f(X) = \left( \frac{9}{8} \right)^{1/3} \cdot \left\{ \left[ 1 - X \left( 1 - \frac{\rho_{H_2}}{\rho_{air}} \right) \right]^{1/3} + (1 - X)^{2/3} \right\}$

# Natural versus passive 2/2

Difference:  $f(X) = \left(\frac{9}{8}\right)^{1/3} \cdot \left\{ \left[ 1 - X \left( 1 - \frac{\rho_{H_2}}{\rho_{air}} \right) \right]^{1/3} + (1 - X)^{2/3} \right\}$



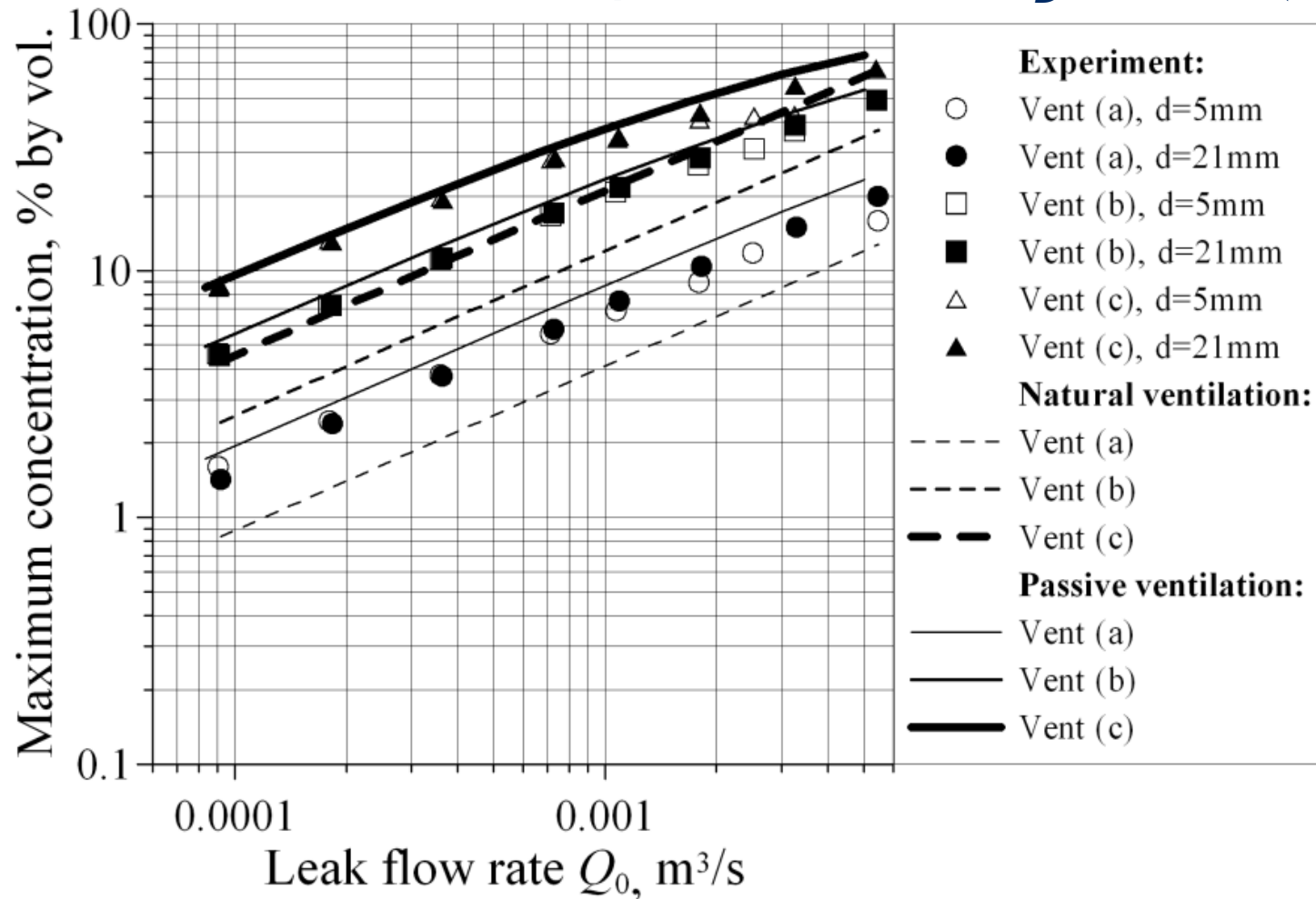
Natural ventilation equation:

- Underestimate **x2 (lean)**
- Overestimate **x2 (rich)**

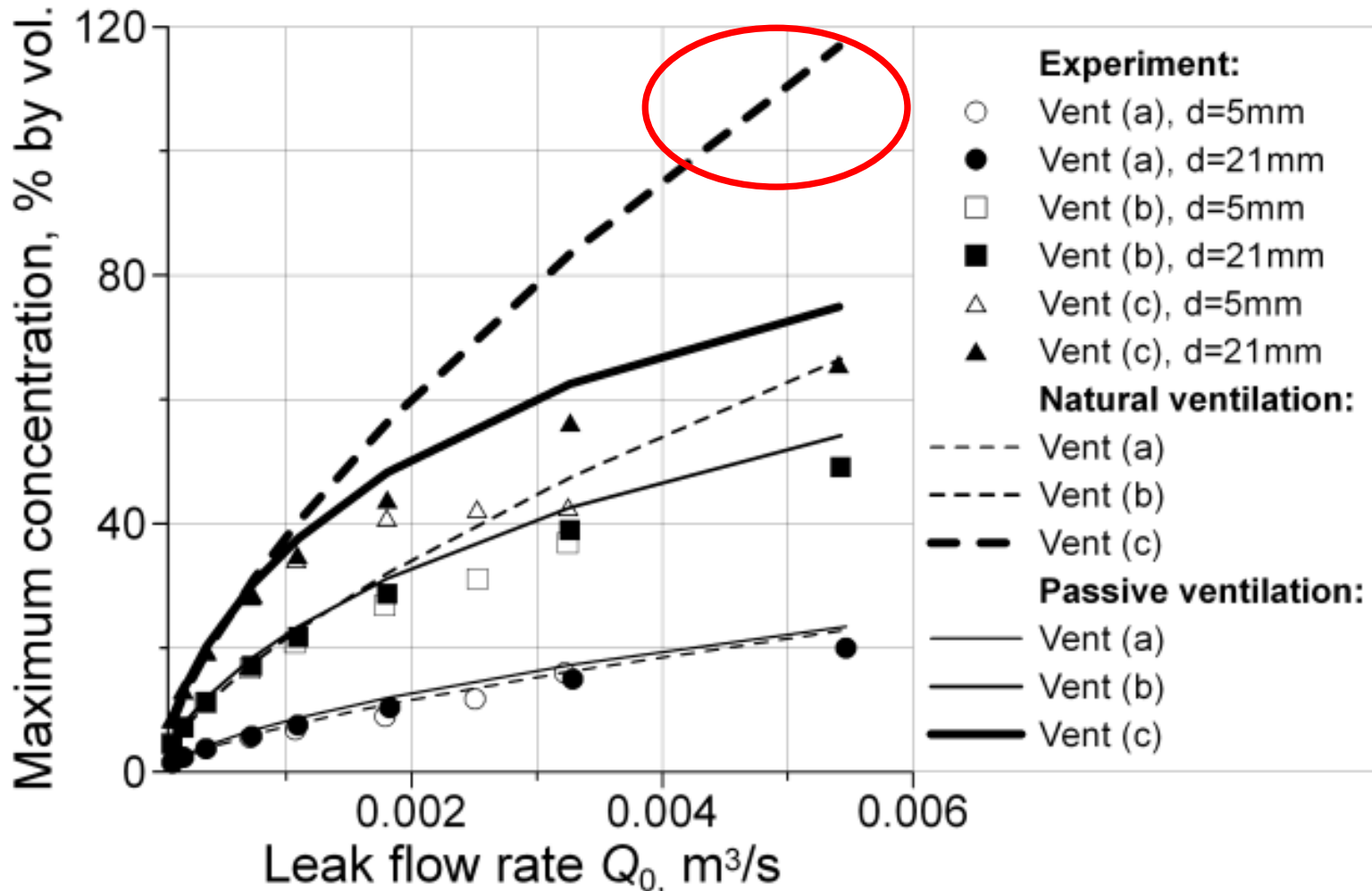
# Validation tests

- Experiments were carried out by CEA (France) within GAMELAN series of experiments using helium released into  $H \times W \times D = 1.26 \times 0.93 \times 0.93$  m enclosure.
- One vent located on a wall near the ceiling.
- Three different vent sizes were studied:
  - vent (a)  $W \times H = 90 \times 18$  cm,
  - vent (b)  $18 \times 18$  cm,
  - vent (c)  $90 \times 3.5$  cm.
- Helium was released upwards from a tube mounted in the centre of the enclosure 21 cm above the floor. Pipes with internal diameter of 5 mm and 21 mm had been used.

Natural ventilation equation with  $C_D=0.60$  (dashed).  
 Passive ventilation equation with  $C_D=0.60$  (solid).

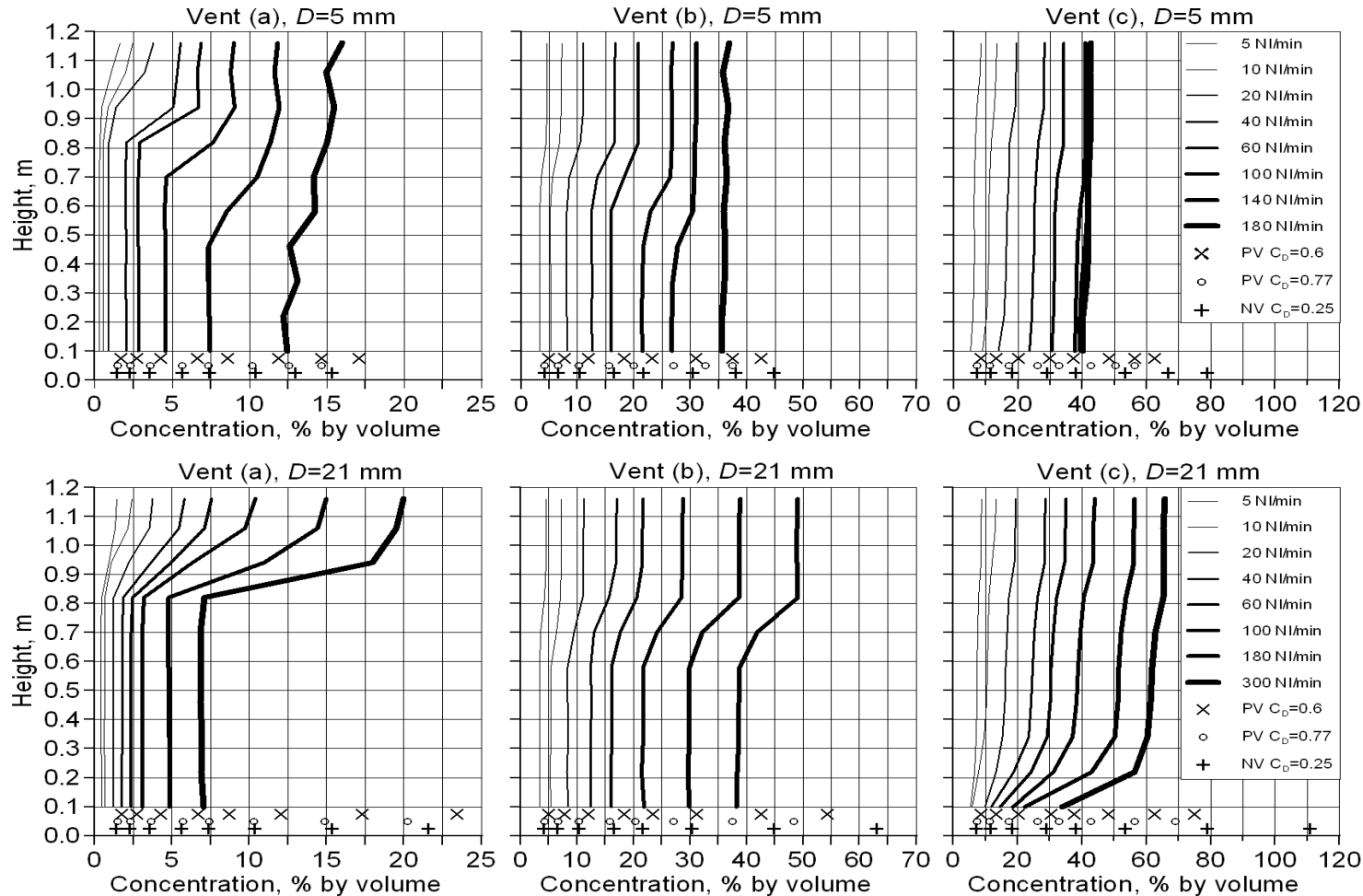


Natural ventilation equation with “tuned”  $C_D=0.25$ .  
 Passive ventilation equation with  $C_D=0.60$ .

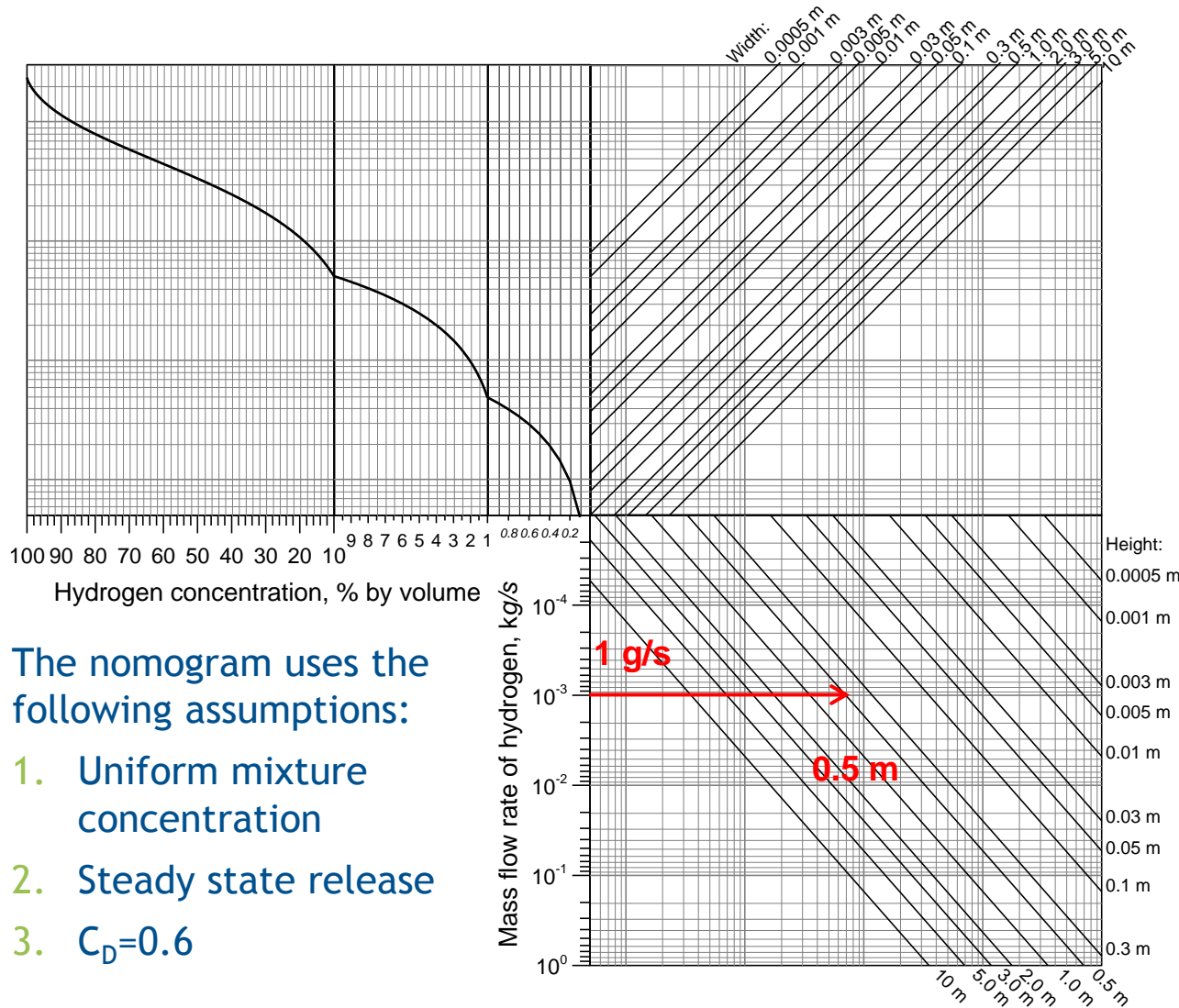




Vent (a): HxW=18x90 cm; Vent (b): 18x18 cm; Vent (c): 3.5x90 cm



# Maximum concentration nomogram



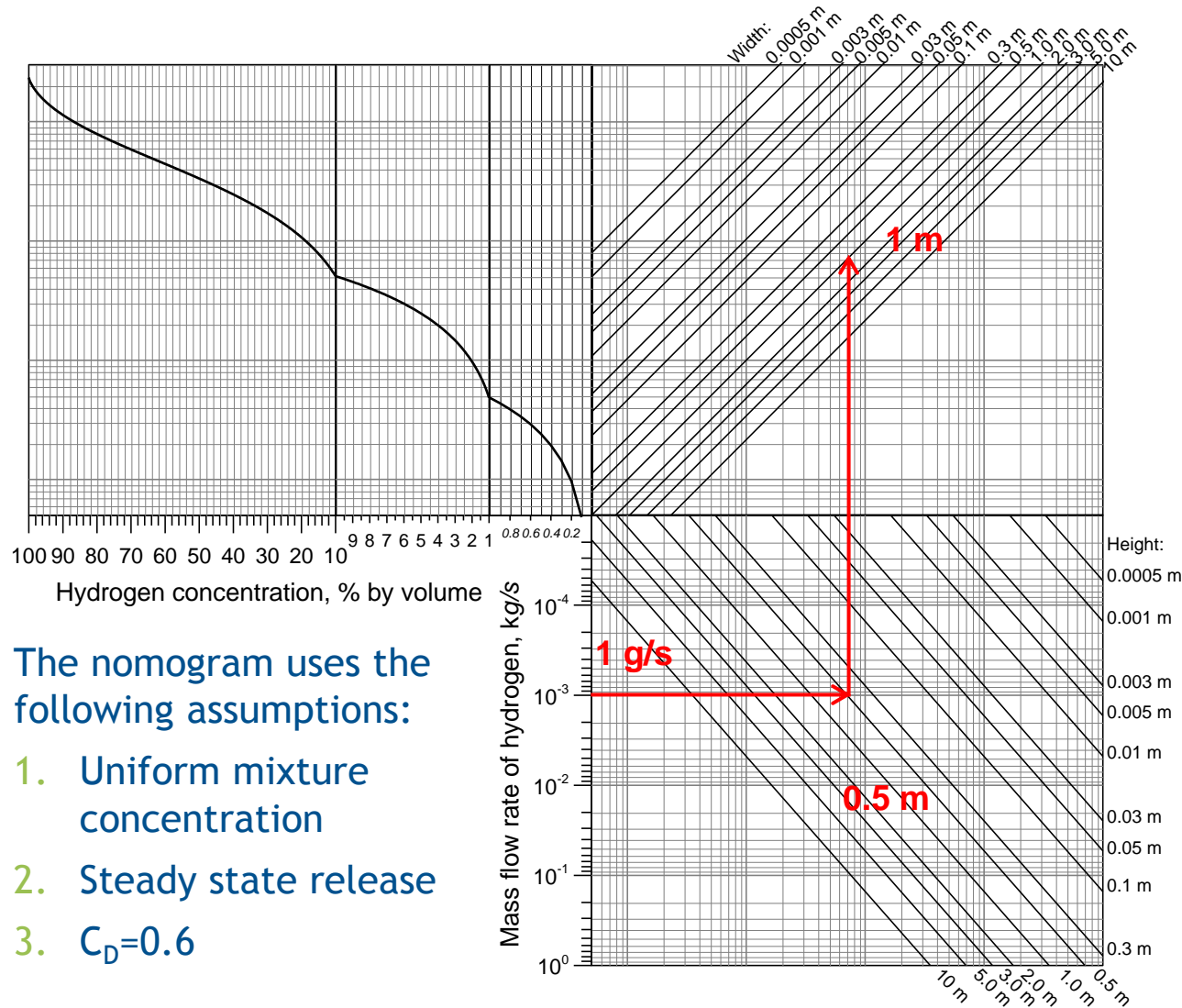
Calculation example 1:

1. Release rate (1 g/s)
2. Vent Height (0.5 m)

The nomogram uses the following assumptions:

1. Uniform mixture concentration
2. Steady state release
3.  $C_D=0.6$

# Maximum concentration nomogram



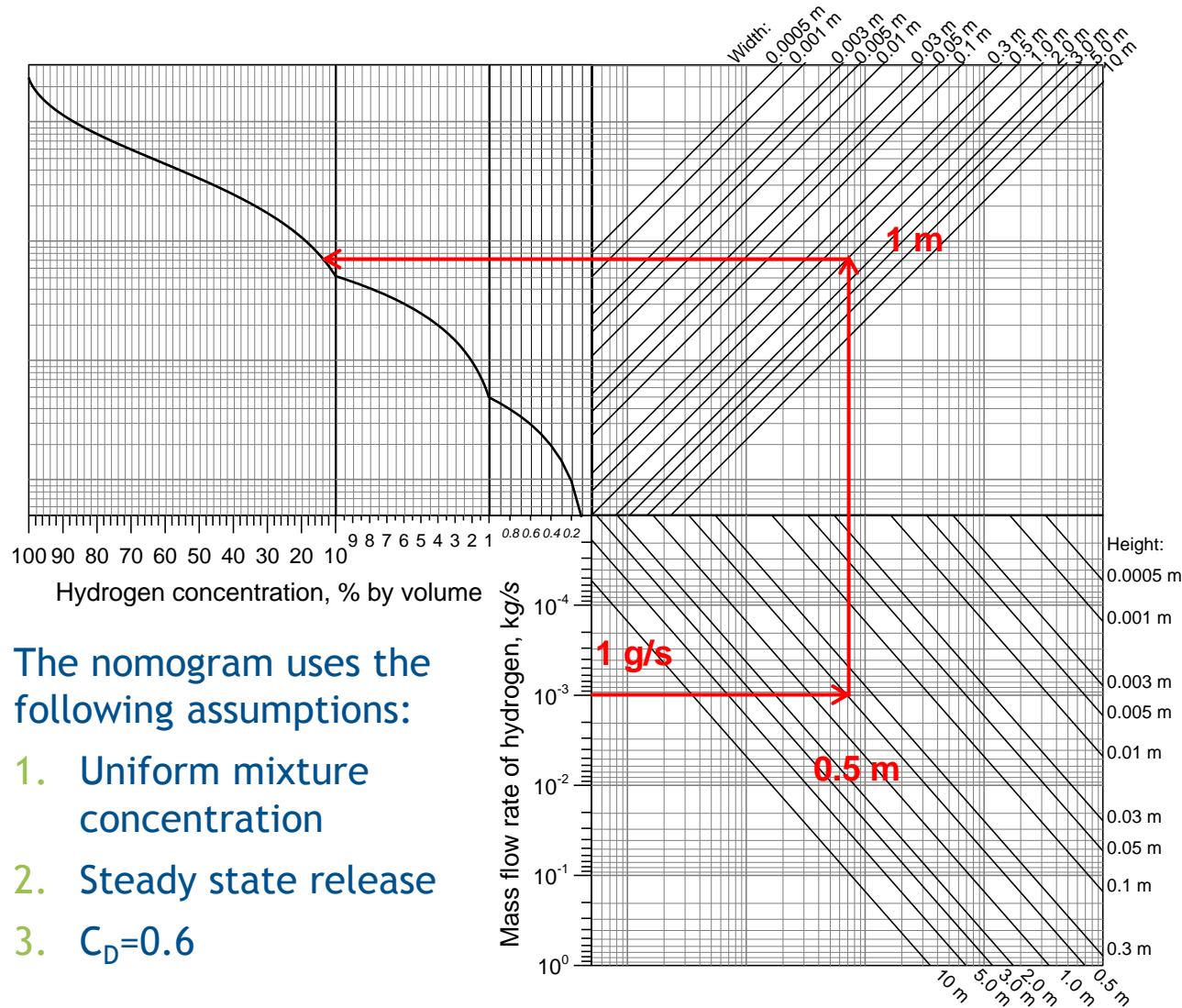
Calculation example 1:

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# Maximum concentration nomogram



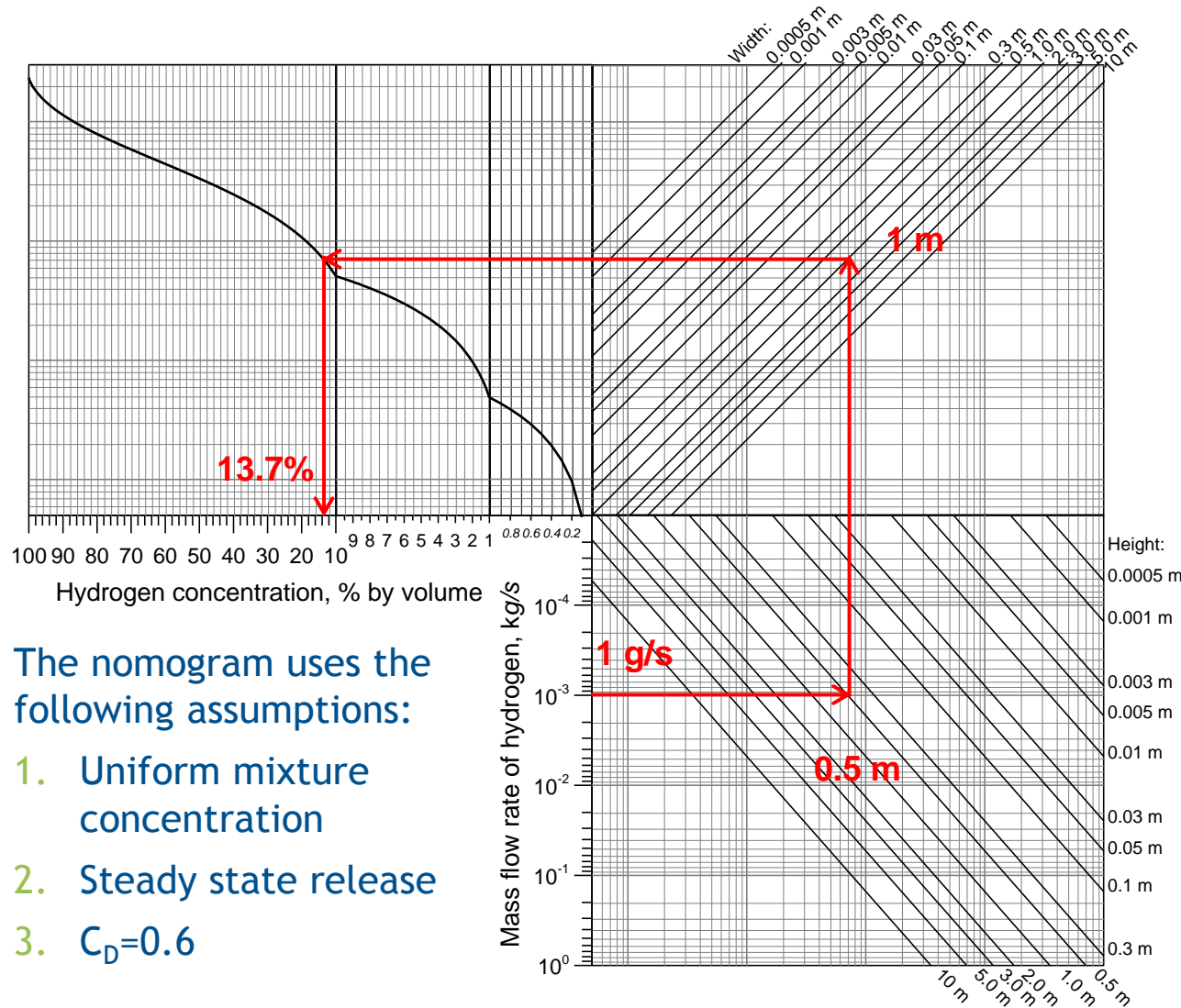
Calculation example 1:

1. Release rate (1 g/s)
2. Vent Height (0.5 m)
3. Vent width (1 m)
4. Function curve

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# Maximum concentration nomogram



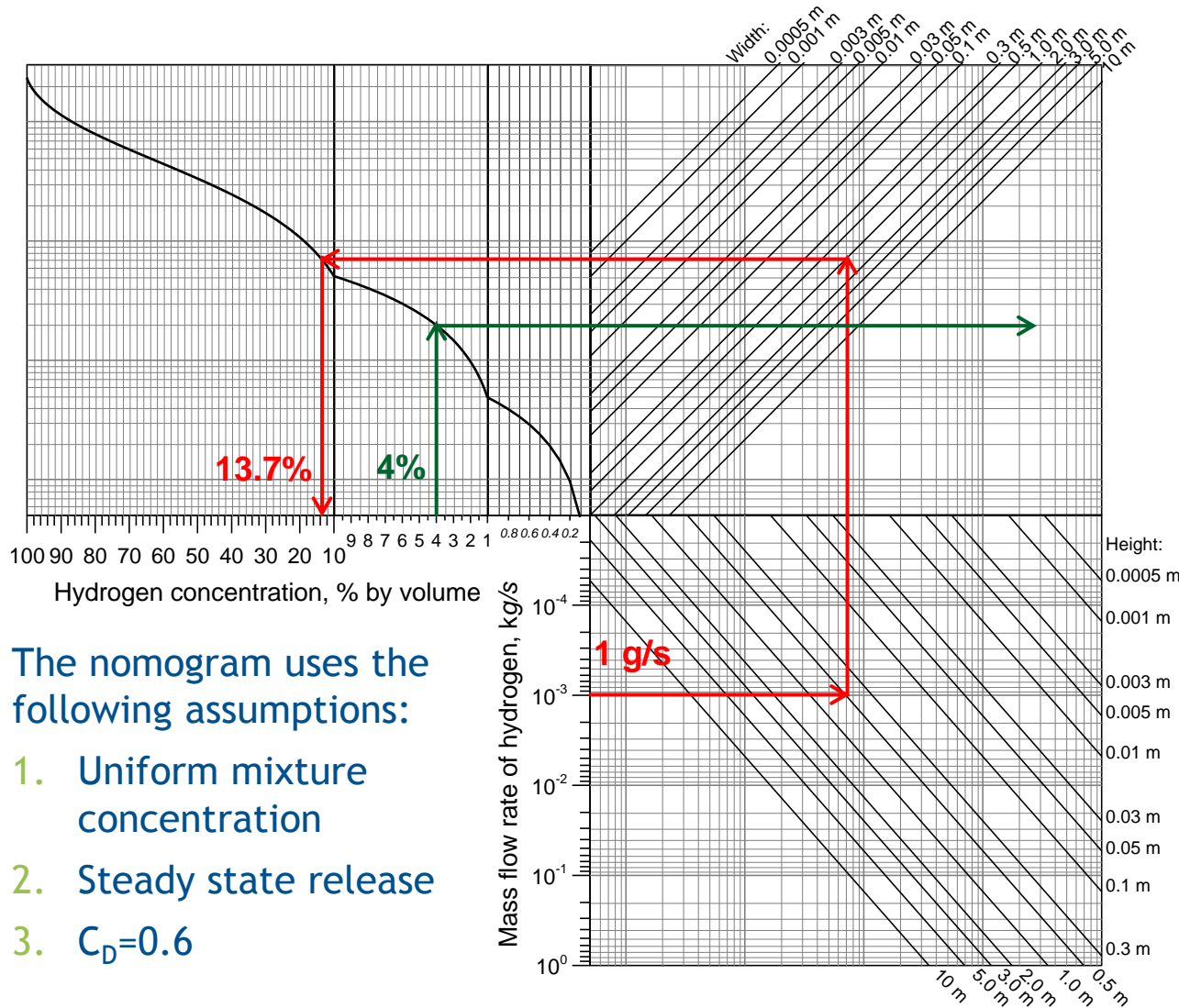
Calculation example 1:

1. Release rate (1 g/s)
2. Vent Height (0.5 m)
3. Vent width (1 m)
4. Function curve
5. Concentration (13.7%)

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# Maximum concentration nomogram



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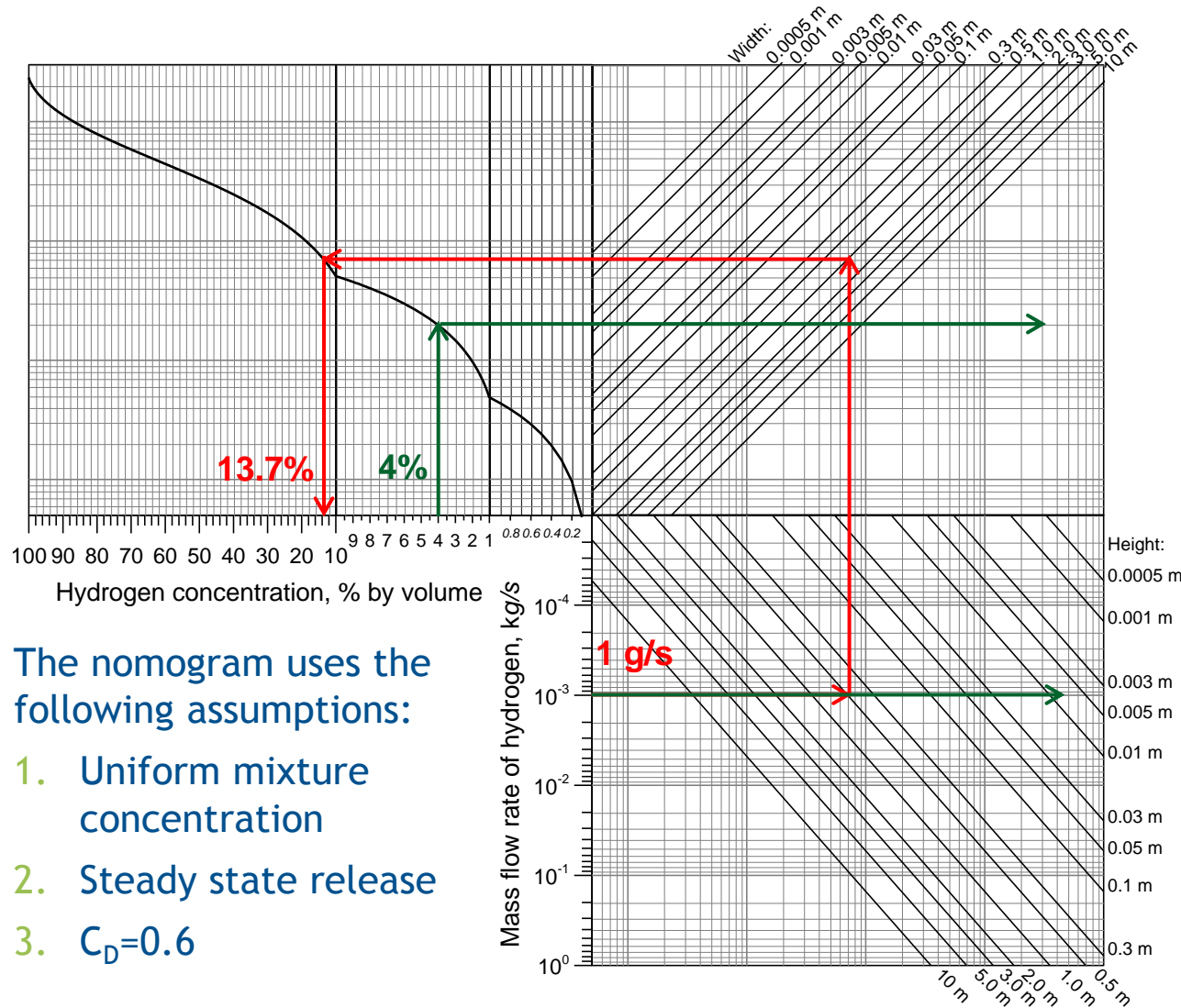
Calculation example 2:

1. Maximum allowable concentration (~4%)
2. Function curve

The nomogram uses the following assumptions:

1. Uniform mixture concentration
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# Maximum concentration nomogram



## Calculation example 1:

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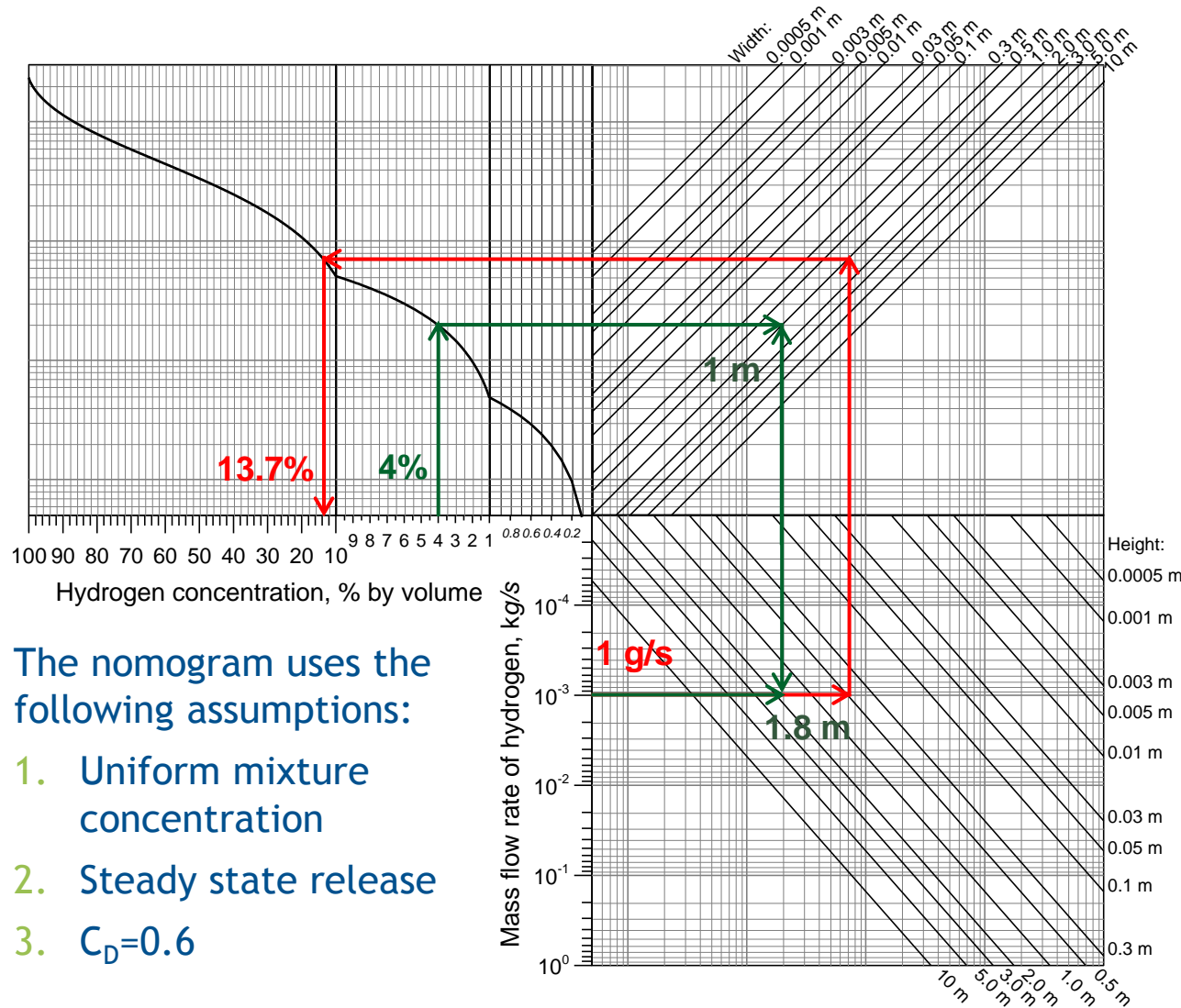
## Calculation example 2:

1. Maximum allowable concentration (~4%)
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3. Release rate (1 g/s)

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# Maximum concentration nomogram



Calculation example 1:

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Calculation example 2:

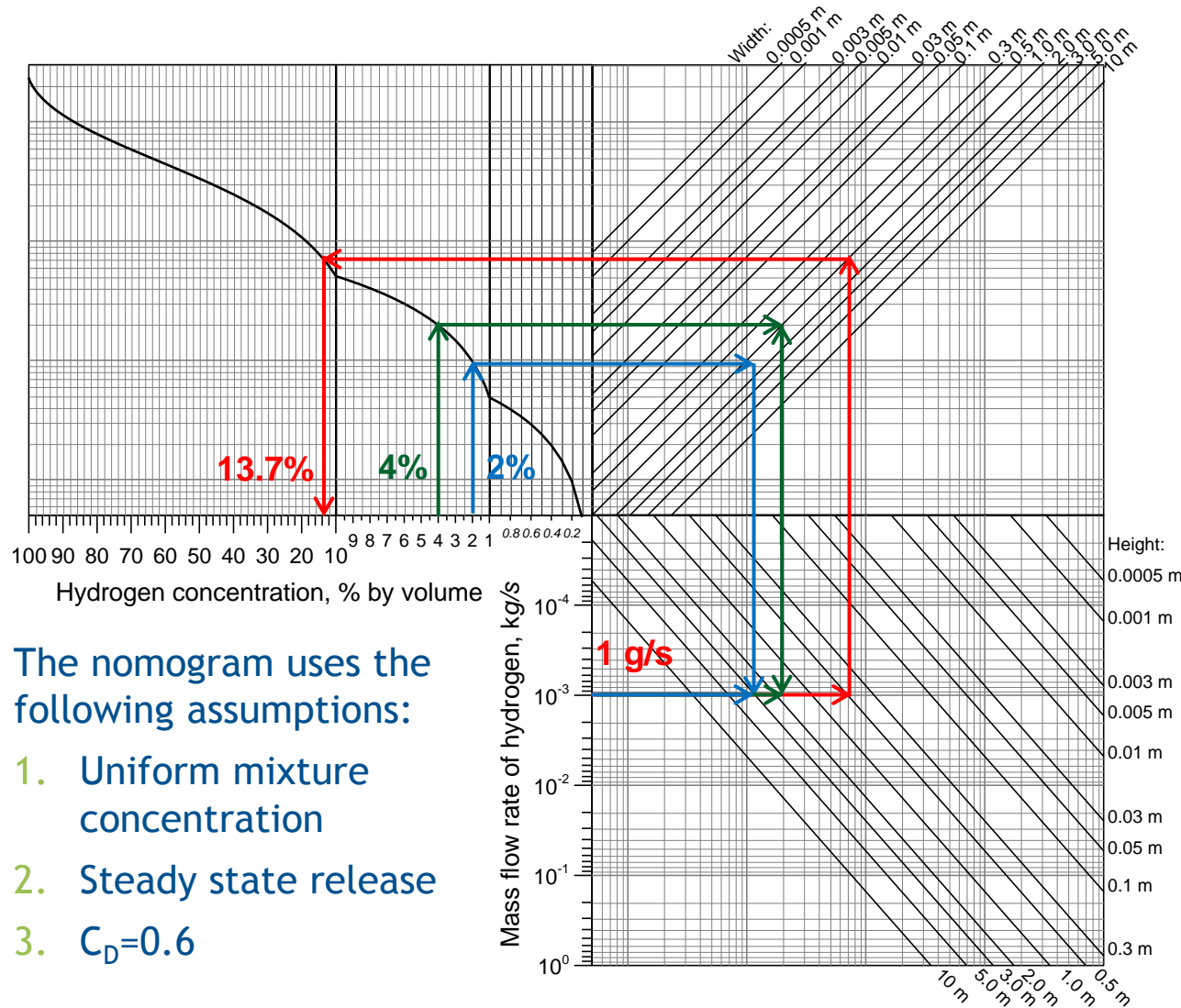
1. Maximum allowable concentration (~4%)
2. Function curve
3. Release rate (1 g/s)
4. Vent height and width (1.8 x 1 m)

The nomogram uses the following assumptions:

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# Maximum concentration nomogram



Calculation example 1:

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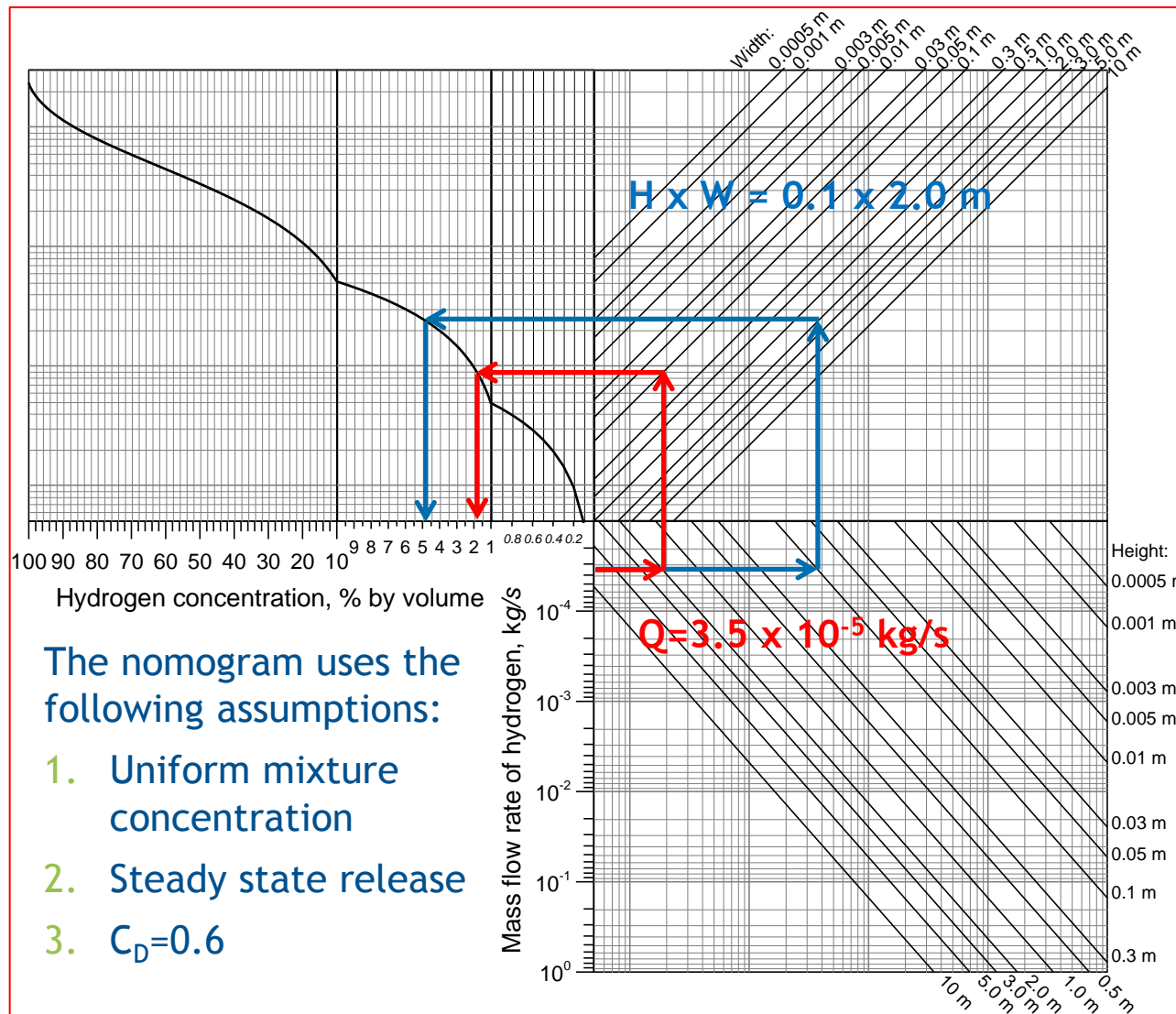
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# Vent orientation effect 1/2



Comparison of 0.2 m<sup>2</sup> vents:

1. Horizontal orientation (H x W = 0.1 x 2.0 m):  
X ~ 4.7% by volume
2. Vertical orientation (H x W = 2.0 x 0.1 m):  
X ~ 1.7 % by volume

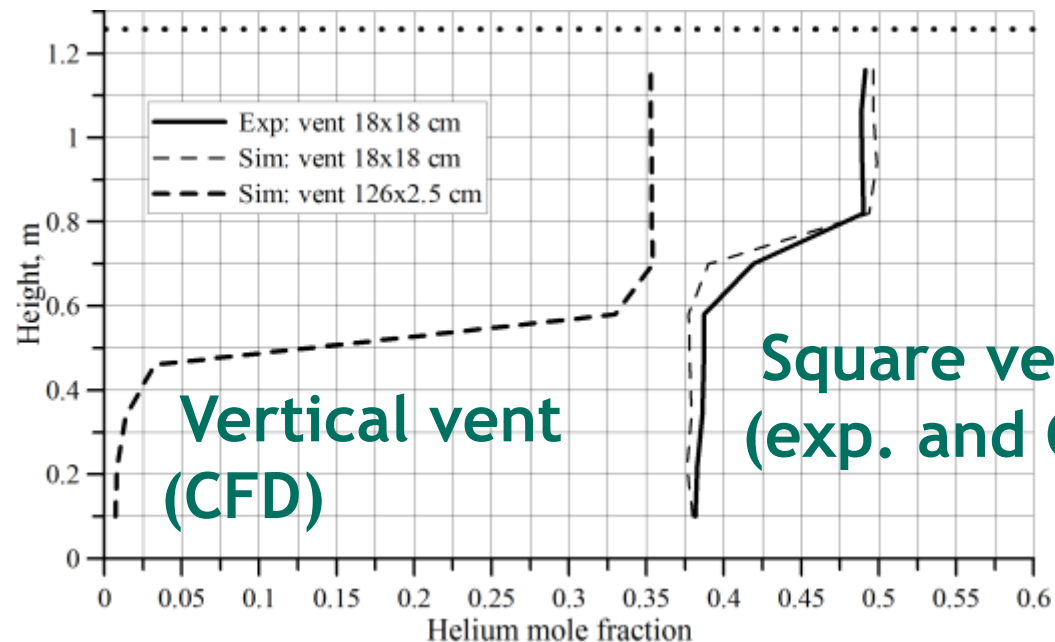
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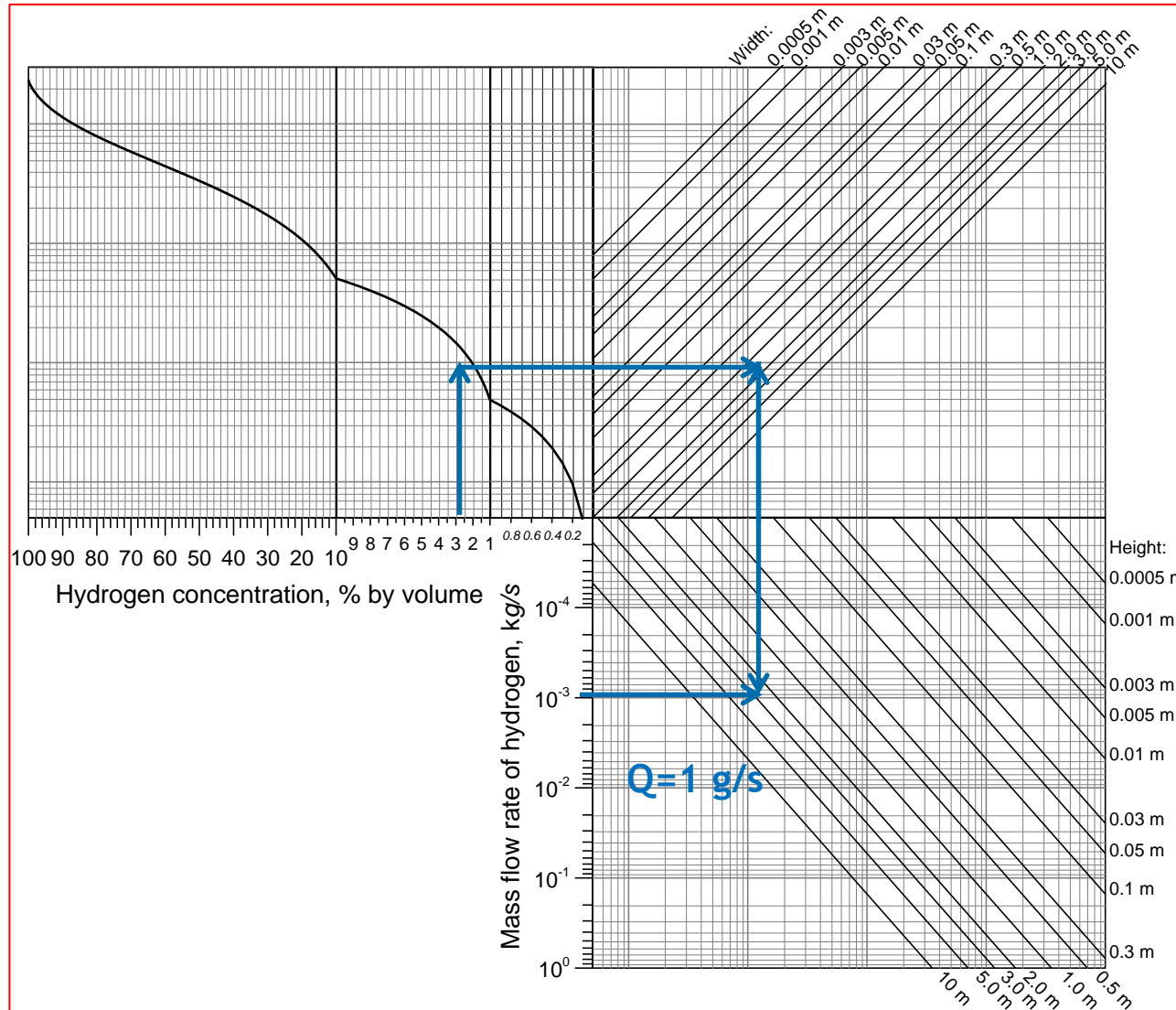
# Vent orientation effect 2/2

Passive ventilation model predicts that for the given vent area vertically oriented vent would be more efficient compared to horizontally oriented (with steady state concentration inversely proportional to  $A\sqrt{H}$  where A is vent area and H is vent height).

Comparison was performed for the 300 NI/min flow rate release from 20 mm diameter pipe. Gamelan experimental data for square vent B (H x W=18 x 18 cm = 0.0324 m<sup>2</sup>) were compared with numerical experiment for the narrow vertical vent B' (H x W = 126 x 2.57 cm) of the same area of 0.0324 m<sup>2</sup>.



# Forced ventilation methodology



Calculation example:

1. Passive ventilation:

2% concentration by volume for 1 g/s release requires unacceptably large 2 x 2 m vent

2. Forced ventilation:

Same steady state concentration can be achieved by replacing single vent with an outlet connected to the forced ventilation, evacuating hydrogen-air mixture at the same flow rate as large passive vent would, and smaller vent connected to atmosphere to allow fresh air. Forced ventilation flow rate can be calculated as  $Q_F = Q_{H_2} / X$  where  $Q_{H_2}$  is hydrogen release rate and  $X$  is hydrogen volume fraction.

For an illustrated example  $Q_F \sim 0.56 \text{ m}^3/\text{s}$

Alternatively, forced ventilation can be used to blow fresh air into the enclosure with the rate  $Q_{FA} = Q_{H_2}(1-X)/X$ . For an illustrated example  $Q_{FA} \sim 0.55 \text{ m}^3/\text{s}$

# Acknowledgements

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